

Review of Flow-Electrode Capacitive Deionization: From Fundamentals to Future Perspectives

Sohair Ahmed Darwish¹, Ibrahim Mohamed Ismail^{1*} and Amr Abdelkader²

¹ Chemical Engineering Department, Faculty of Engineering, Cairo University, Giza 12613, Egypt.

² Mechanical Engineering Department, Faculty of Engineering, British University in Egypt, El-Sherouk 11837, Cairo, Egypt Received: 5 Aug. 2024, Revised: 18 Sep. 2024, Accepted: 21 Oct. 2024.

Received: 5 Aug. 2024, Revised: 18 Sep. 2024, Accepted: 21 Oct. 2024.

Published online: 1 Jan. 2025.

Abstract: Flow Capacitive Deionization (FCDI) has emerged as an innovative electrically driven separation technology with distinct advantages over conventional desalination methods. Utilising flowable carbon electrodes and ion exchange membranes, FCDI enables continuous operation, high water recovery, and selective ion removal at relatively low energy consumption. This review critically examines the historical development, operational mechanisms, cell architectures, and configurations of FCDI systems, with particular focus on recent advances in materials, flow-electrode formulation, and regeneration strategies. This review also highlights emerging opportunities for FCDI in selective ion recovery and resource extraction. Despite its promise, FCDI remains at a pre-commercial stage due to high capital costs and system complexity. Ultimately, progress in advanced materials, system modelling, and scalable cell design will be essential to realise its transition from laboratory innovation to a commercially viable solution for sustainable water treatment.

Keywords: Flow-Electrode Capacitive Deionization, Flow-Electrode, Electrosorption, Desalination.

1 Introduction

Over the past ten years, Capacitive Deionization (CDI) technologies have received significant attention [1]. In these processes, ions are transported to the oppositely charged electrodes by applying potential difference. Then, ions are adsorbed within the electrode material. Porous carbon electrodes are typically used to achieve high surface areas and, hence, high capacity of ion adsorption [2].

The addition of Ion-Exchange Membranes (IEMs) to CDI innovated a new configuration known as Membrane Capacitive Deionization (MCDI), makes CDI processes more energy-efficient with improved desalination performance [3], benefiting from the IEMs' ability to selectively permit counter-ion transport while effectively suppressing the back-diffusion of co-ions into the feedwater compartment [4]. This effect is particularly advantageous at low salinity levels, where co-ion leakage would otherwise diminish the ion removal capacity of conventional CDI [2].

All solid electrodes used in CDI and MCDI systems are immobile and become progressively saturated with ions during operation [5]. As a result, these electrodes require periodic regeneration through desorption, necessitating discontinuous operation in the form of charge-discharge cycles [6]. This cyclic nature, along with the depletable ion storage capacity of fixed electrodes, restricts the practical applicability of CDI and MCDI technologies to feedwaters with relatively low salinity levels [1].

A new technology based on capacitive deionization and flow capacitor systems [8] is Flow-Electrode Capacitive Deionization (FCDI). Unlike CDI and MCDI, which utilise solid and static stationary carbon electrodes, FCDI employs fluidised, pumpable carbon suspensions, referred to as flow or slurry electrodes [9], as illustrated in Figure 1.

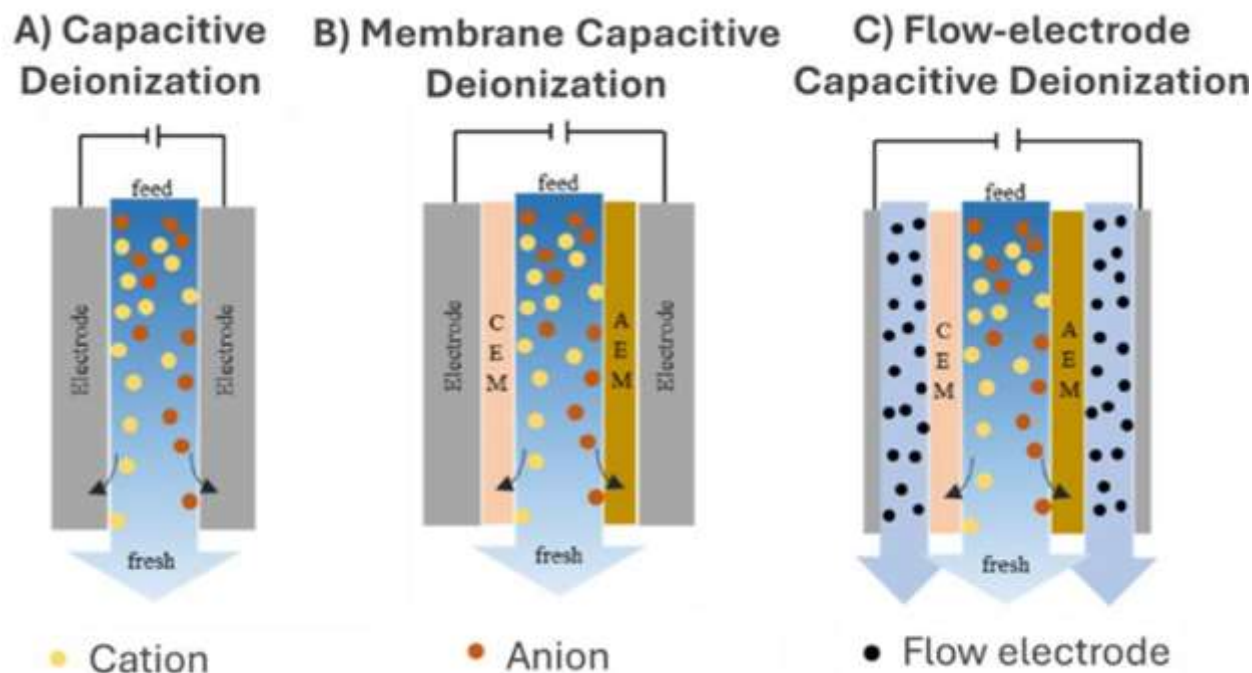


Fig. 1: Schematic diagrams of (a) Capacitive Deionization (CDI); (b) Membrane Capacitive Deionization (MCDI); and (c) Flow-Electrode Capacitive Deionization (FCDI) [7].

Upon applying an electrical potential, ions in the feed migrate across IEMs and are adsorbed onto the surface of the carbon particles [10]. These charged flow electrodes can then be continuously transported out of the desalination cell to a separate regeneration unit, allowing for uninterrupted continuous operation and sustained ion removal performance [11]. Overall, FCDI is positioned as a promising technology due to the high salt adsorption capacities [11,12], good desalination performance [12], and the continuous operation [11,14,15].

This review article provides an overview of FCDI technology. It begins with FCDI's history, principle of operation and mechanism, followed by the system's design, including cell architecture, electrode materials, separator materials, and operational modes. Some emerging applications of FCDI beyond desalination are also presented. Finally, current commercialisation status, challenges, and the future outlook of FCDI are discussed.

2 Historical Developments and Evolution

FCDI is a relatively recent innovation that evolved from foundational concepts first explored in the 1960s. The concept of "electrochemical demineralization" or "electrosorption" of water was first reported by Blair and Murphy in 1960 [16]. Early studies by Johnson and Newman in 1971 laid the groundwork for ion electrosorption using carbon electrodes [17]. However, it wasn't until the 1990s that CDI gained renewed attention with the development of advanced porous carbon materials such as carbon aerogels [18]. The membrane-enhanced CDI (MCDI) was introduced in 2004 [3], integrating ion-exchange membranes to enhance ion selectivity and charge efficiency, laying groundwork for future advancements.

FCDI was pioneered in 2013 by Jeon et al. [13], as a response to inherent limitations of CDI and MCDI, particularly their batch-mode operation and limited salt removal capacity. The key innovation was the use of flowable carbon slurry electrodes that could be regenerated outside the desalination cell, enabling continuous operation without the interruption of periodic electrode regeneration. This breakthrough sparked a wave of innovation, with subsequent advancements in both design and application [19].

Since then, research focused on optimising desalination performance by innovating the flow electrodes through exploring various carbon materials and improving their conductivity, stability, and flowability [19,20]. Concurrently, system-level enhancements were introduced, including improved cell geometries and innovative regeneration schemes which allow for energy recovery and stable continuous performance [10,21,22].

By the late 2010s, FCDI systems were successfully demonstrated for selective ion removal [23]. Studies also confirmed FCDI's ability to operate at high water recovery and handle higher salinity feeds, making it a strong candidate for brine concentration applications [24]. Modelling and simulation work matured in parallel, offering insights into the combined electrodialytic and capacitive mechanisms and enabling performance prediction under various operational modes [25].

In the early 2020s, the scope of FCDI research broadened significantly. The technology was applied to emerging areas such as resource recovery (nutrients and valuable ions) and contaminant removal (organic and heavy metals) [19]. Today, FCDI remains a pre-commercial but rapidly advancing technology [26]. Its continuous operation, high recovery, tunable selectivity, and relatively low energy consumption, all position it as a compelling candidate for future desalination and resource recovery systems [19,27].

3 Principle of Operation and Advantages

FCDI was proposed to overcome several limitations of traditional CDI and MCDI systems by replacing the fixed porous electrodes with dynamic, pumpable carbon suspensions that circulate through designated channels on the current collectors [13]. This configuration allows ions to be continuously removed from the feed solution and adsorbed onto the surface of flowing carbon particles via the formation of electric double layer [28].

A standard FCDI module, illustrated in Figure 2, typically consists of three compartments: two outer electrode chambers (one for the cathode and one for the anode), and a central water chamber. The electrode compartments house the carbon-based slurry, while the central channel contains a spacer to allow feed flow. The electrode and water compartments are separated by IEMs, or any porous separating material [19].

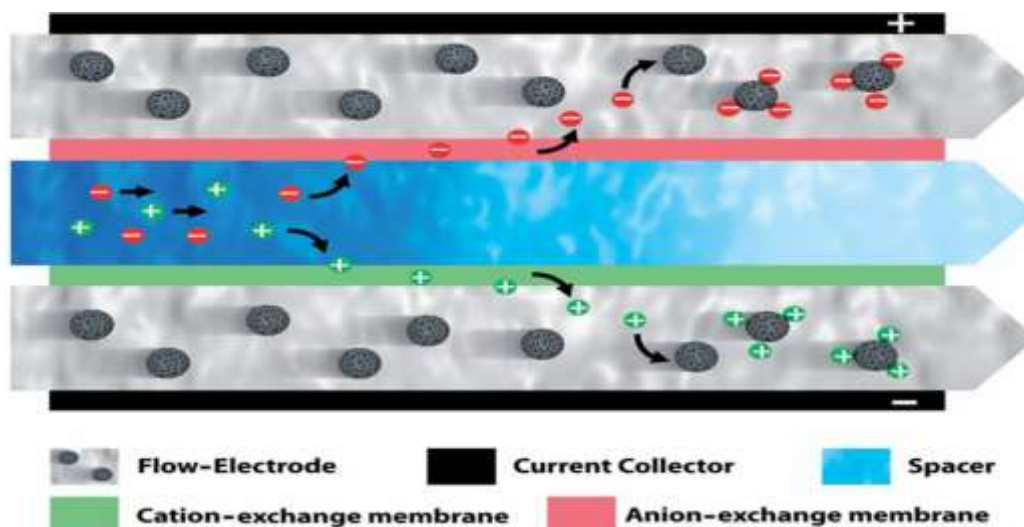


Fig. 2: Schematic representation of a typical FCDI cell [29].

When a low electric potential (~ 1.2 V) is applied, cations and anions migrate across the separating material towards oppositely charged flow electrodes, where they are electrostatically adsorbed [30]. This process resembles that of static CDI, but with a key distinction: the charge/discharge cycles occur outside the main desalination cell. The used flow-electrodes from the cathodic and anodic chambers are pumped into an external regeneration unit, where the oppositely charged suspensions are mixed, allowing spontaneous neutralization and salt release [13]. The regenerated carbon suspensions are then recirculated into the electrode compartments, enabling continuous operation. This arrangement supports a steady-state operation in which the compositions of effluent streams remain constant over time [31].

The unique configuration of FCDI leads to several operational advantages. Unlike static CDI or MCDI, where electrode saturation limits the cycle duration, FCDI offers continuous operation, reducing downtime and enhancing overall desalination efficiency. The ability to regenerate electrodes externally makes the process inherently more scalable, as performance can be improved simply by increasing the flow-electrode volume [13]. Additionally, the external regeneration system opens opportunities for energy recovery, as the mixing of oppositely charged suspensions can theoretically produce usable energy [31].

Studies have also shown that FCDI can achieve higher salt removal rates and maintain more consistent ion removal performance than traditional CDI systems, especially over long durations. FCDI's ability to desalinate high salinity feeds has been well reported in literature [32,33].

Compared to electrodialysis (ED), FCDI performs competitively in treating complex water chemistries and brackish water, with the added benefit of potentially lower energy consumption in certain scenarios. Furthermore, flow electrodes are less prone to fouling compared to stationary electrodes, as the continuous movement of the slurry helps minimise foulant accumulation on the surface of suspended carbon particles [34]. Although FCDI may not yet compete with the energy efficiency of RO, particularly of large-scale systems, it is more modular and requires less infrastructure, making it suitable for decentralized and flexible water treatment applications [19].

The comparison in Table 1 reveals that FCDI outperforms conventional capacitive technologies and electrodialysis in several critical aspects, with its main advantages include: i) continuous desalination enabled by external electrode regeneration

- ii) Enhanced ion adsorption capacity and salt removal performance
- iii) Potential for energy recovery during flow-electrode regeneration
- iv) Ability to desalinate water with higher salinity levels
- v) High scalability through increasing flow-electrode volume
- vi) Ability to handle complex water chemistries while resisting fouling
- vii) Modular and decentralised design

These features underline FCDI's potential for industrial-scale applications and position it as a promising candidate for next-generation desalination systems.

Table 1: Comparison of the key features and limitations of electrically driven desalination technologies [35,36,37,38].

Parameter	CDI	MCDI	FCDI	ED
Mode	Intermittent	Intermittent	Continuous	Continuous
Cell Complexity	Simple	Moderate	Complex	Complex
Charge efficiency	Low	Low to Moderate	High	Moderate to High

Salt Removal Capacity	Low	Low	High	High
Fouling Tolerance	Poor	Moderate	High	Poor
Ion selectivity	Limited	Improved with IEMs	Tunable (electrode design)	Fixed (by membrane type)
Key limitation	Low capacity and low salinity limit	Non-continuous operation	Risk of electrode clogging	Water splitting leading to pH shifts
Maturity level	Commercial	Commercial	Emerging	Industrial
Brine treatment feasibility	Not feasible	Not preferred	Promising	Possible

4 Mechanism and Advanced Operating Principles

The performance of FCDI is governed by electrochemical and mass transport phenomena that underpin both ion removal and charge transfer processes. This section provides a detailed explanation of the core mechanisms that define FCDI operation, focusing on ion storage within the flow-electrode and the associated mechanisms of charge transport. A clear understanding of these principles is essential for optimising system design, improving salt removal capacity, and tailoring electrode and cell configurations for advanced performance.

4.1 Ion Storage Mechanisms

4.1.1 Capacitive Ion Storage

In CDI technologies, ion removal is fundamentally driven by the formation of Electrical Double Layers (EDLs) on the surfaces of porous carbon materials [39]. Upon the application of an external voltage, ions in the feedwater migrate toward the oppositely charged electrode and are electrostatically adsorbed, forming EDLs on the accessible electrode surfaces [40]. Figure 3 illustrates commonly used EDL models, with a focus on the structure around a positively charged electrode [19].

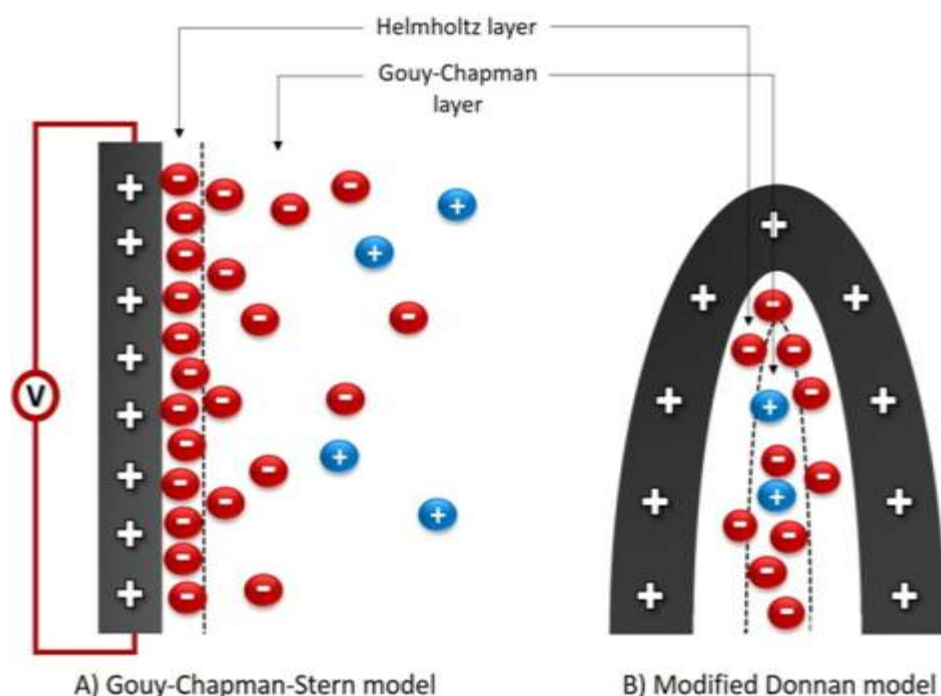


Fig. 3: Models explaining EDL formation and ion distribution [23].

The classical Gouy-Chapman-Stern model describes the EDL [41] as a combination of two distinct regions: 1) a compact layer where ions of the opposite charge are electrostatically accumulated close to the charged electrode's surface, followed by 2) a diffuse ion cloud, where ions disperse farther away [19].

Since CDI technologies primarily employ microporous electrodes [42,43], the applicability of the Gouy-Chapman-Stern model becomes limited. Instead, the modified Donnan model offers a more suitable theoretical framework, as it accounts for the overlapping of EDL within finite pores [44]. This mechanism emphasizes the importance of using materials with high surface area and porosity to enhance ion adsorption efficiency [45].

4.1.2 Faradic Ion Storage

FCDI technology can facilitate both capacitive and Faradaic ion storage mechanisms, depending on variables such as the electrode material and the magnitude of the applied electrical potential. Nonetheless, Faradaic side reactions are typically unintended and remain relatively minor under standard operating conditions [46].

Upon applying a voltage difference, minor Faradaic side reactions may occur on the surface electrodes, such as carbon oxidation or water electrolysis, leading to pH changes in the electrolyte [47]. Although FCDI operates under relatively low voltages, faradaic reactions still occur during the process [48]. However, capacitive ion storage is the dominating mechanism in CDI processes under typical operating voltages (~ 1.2 V) and when standard carbon electrodes are employed [19].

In contrast, Faradaic ion storage mechanisms, such as redox reactions or ion intercalation, only become significant when using redox-active electrodes (such as transition metal oxides or conductive polymers) [49] or operating at higher voltages. These are typically associated with pseudocapacitive or hybrid CDI configurations, where at least one electrode is designed to engage in Faradaic processes. Such hybrid systems are being actively explored for their enhanced ion removal capacity, but they differ fundamentally from conventional FCDI systems [19].

4.1.3 Ion Storage Under Flow Conditions

A unique characteristic of FCDI is that even while carbon particles are in motion within the slurry, the suspension remains electrically conductive, and the EDLs on the particles persist during flow [31]. In fact, from a theoretical standpoint, the equilibrium electrosorption capacity of the carbon particles should remain the same regardless of whether the system is in a flow or static configuration [50]. Figure 4 illustrates the charge storage mechanism within a flow electrode system. In this configuration, a carbon-electrolyte suspension is circulated between two polarised current collectors, where ions from the electrolyte migrate to counterbalance the surface charges on the suspended carbon particles, allowing energy to be stored in the EDL during operation.

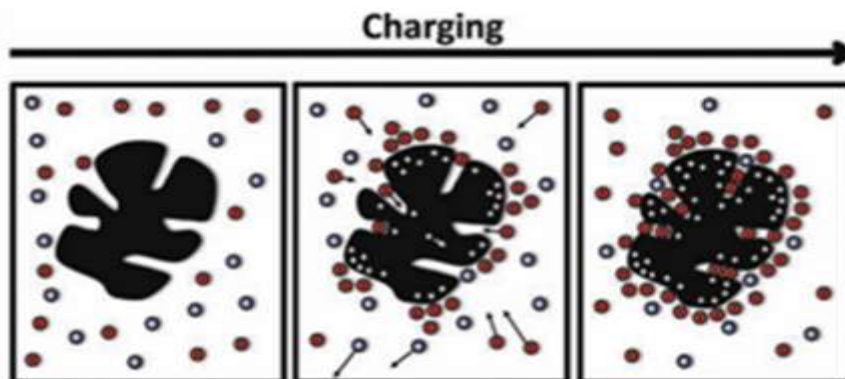


Fig. 4: Ion storage mechanism of flow electrode in FCDI [50].

4.2 Charge transport in flow-electrode

Charge transport in the flow-electrode includes the transport of both electrons and ions, as shown below in Figure 5. Electron transport occurs via three primary pathways: 1) direct contact between the carbon particles and the current collector, 2) conduction via a continuous network of physically connected carbon particles, and 3) transfer facilitated by redox reactions between particles, requiring the addition of a redox-active species in the flow-electrode. Meanwhile, ion transport occurs through two pathways: 4) through the bulk electrolyte along the surface of the particles, or via 5) migration within the EDLs surrounding the particles [51].

A deeper understanding of charge transport mechanisms within flow-electrodes are essential for enhancing FCDI desalination. It is widely accepted that electron percolation is highly dependent on the extent and quality of physical contact between conductive particles. Studies found that increasing the carbon content improved the connectivity between particles, hence it made electron movement more directional, but it also made ion movement more complex and indirect [51].

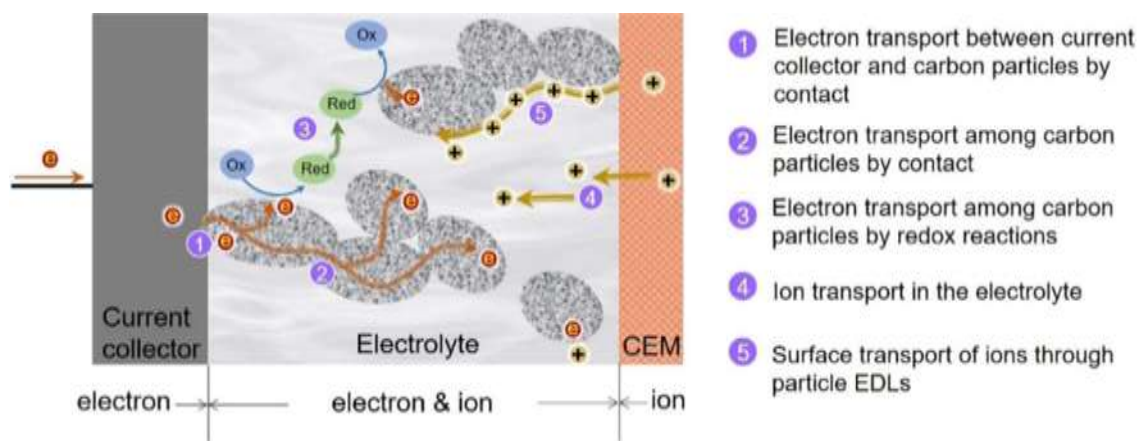


Fig. 5: Main charge transport mechanisms in flow-electrodes in FCDI [51].

4.3 Effect of Applied potential

The influence of applied voltage variation has been a central focus since the early development of CDI technology [52], and research continues to explore its effect for the optimisation of FCDI cell operation [53].

Recent investigations into the voltage-current characteristics revealed that increasing the applied voltage substantially enhances ion removal efficiency. This outcome can be readily explained through the lens of the EDL theory: higher applied voltage results in greater accumulation of surface charge on the electrode, thereby increasing adsorption capacity. However, the applied voltage must be limited to avoid water electrolysis. Given that the standard potential of water electrolysis is 1.23 V, studies restrict the operating voltage to around 1.2 V [54].

Electrochemical reactions associated with different applied potentials have also been examined by tracking pH variations during adsorption and desorption. These studies showed that the solution pH changed with applied voltage. For instance, at 1.0 V, the pH increases due to dissolved oxygen reduction, whereas at voltages >1.2 V, pH drops rapidly due to chloride oxidation at the anode. Specifically, applying 1.2 V can cause the pH to rise to 10 and decline to below 8 [55].

5 Cell Design

While the critical roles of electrode and membrane design are well acknowledged, it is equally important to emphasise the significance of overall system design. A commonly adopted configuration is depicted in Figure 6, which illustrates the primary components of a typical FCDI cell.

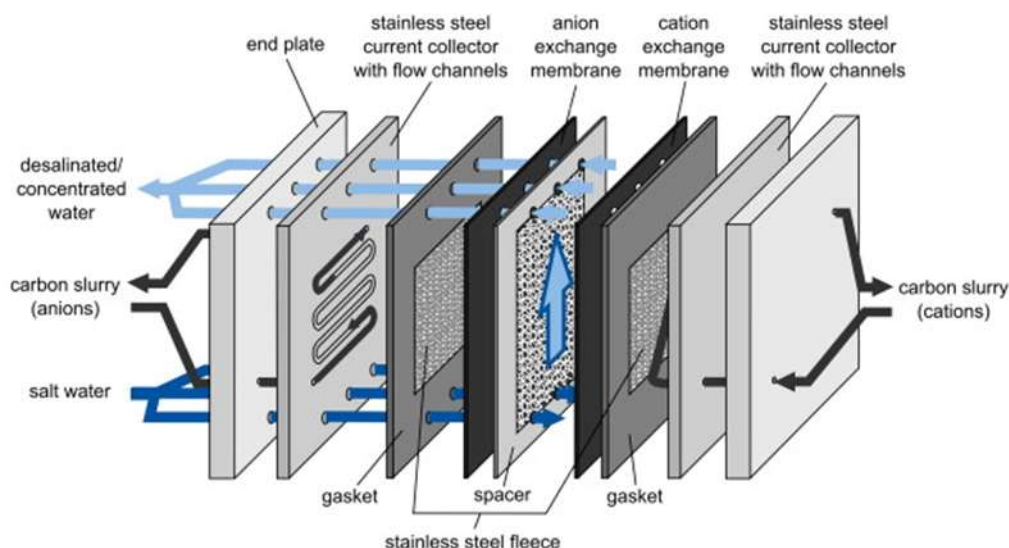


Fig. 6: Structure and components of conventional FCDI module [14].

Since Jeon et al. revolutionised the CDI cell architecture by introducing the flow-electrode concept, researchers have concentrated on optimising the design and functionality of each module component to improve the system's performance, longevity, and cost-efficiency [19]. The following section highlights several significant advancements that have emerged in this context.

5.1 Cell Architecture

The different FCDI cell architectures and designs can be divided into single- or dual-channel cells according to the number of outlet channels (excluding the flow-electrodes), as illustrated in Figure 7.

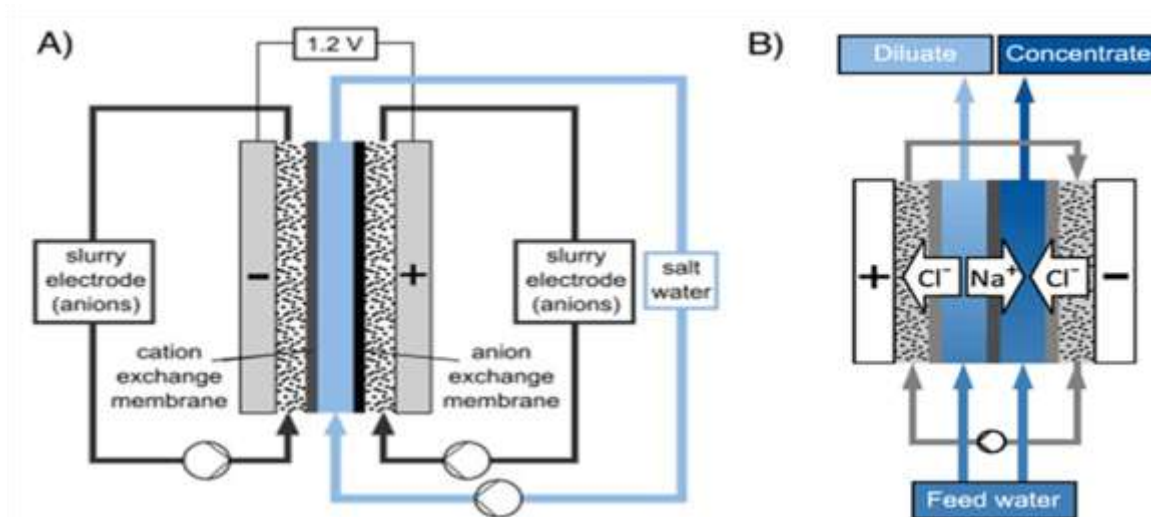


Fig. 7: Structure of (a) single-channel FCDI cell [11] and (b) dual-channel FCDI cell [24].

In a single-channel FCDI cell, the slurry electrode circulates through a serpentine flow path embedded in the current collector and enters the cell for ion adsorption [13]. The adsorbed ions can subsequently be desorbed by either neutralising the charge or applying a reverse potential, followed by electrode regeneration using standard techniques such as settling or filtration [11]. Although this configuration features a relatively simple design, it does

not allow for simultaneous desalination and concentration processes. This limitation is effectively addressed by the dual-channel FCDI cell design.

In a dual-channel FCDI cell, the incoming saltwater is split into two streams, each flowing through separate channels divided by an IEM, facilitating simultaneous desalination and concentration. The electrode that adsorbs a specific type of ion is circulated to the opposite chamber for ion release [24]. This configuration bears resemblance to ED systems [19]. A key advantage of this cell design is its ability to produce two distinct outlet streams simultaneously (one of desalinated water and the other of concentrated brine) enabling continuous and efficient operation.

Other innovative cell arrangements have been reported in literature. For instance, although the majority of FCDI cells have a planar configuration, Porada et al. [31] introduced a design that incorporates tubular IEMs, illustrated in Figure 8. This new configuration not only enabled continuous desalination, but also continuous energy recovery.

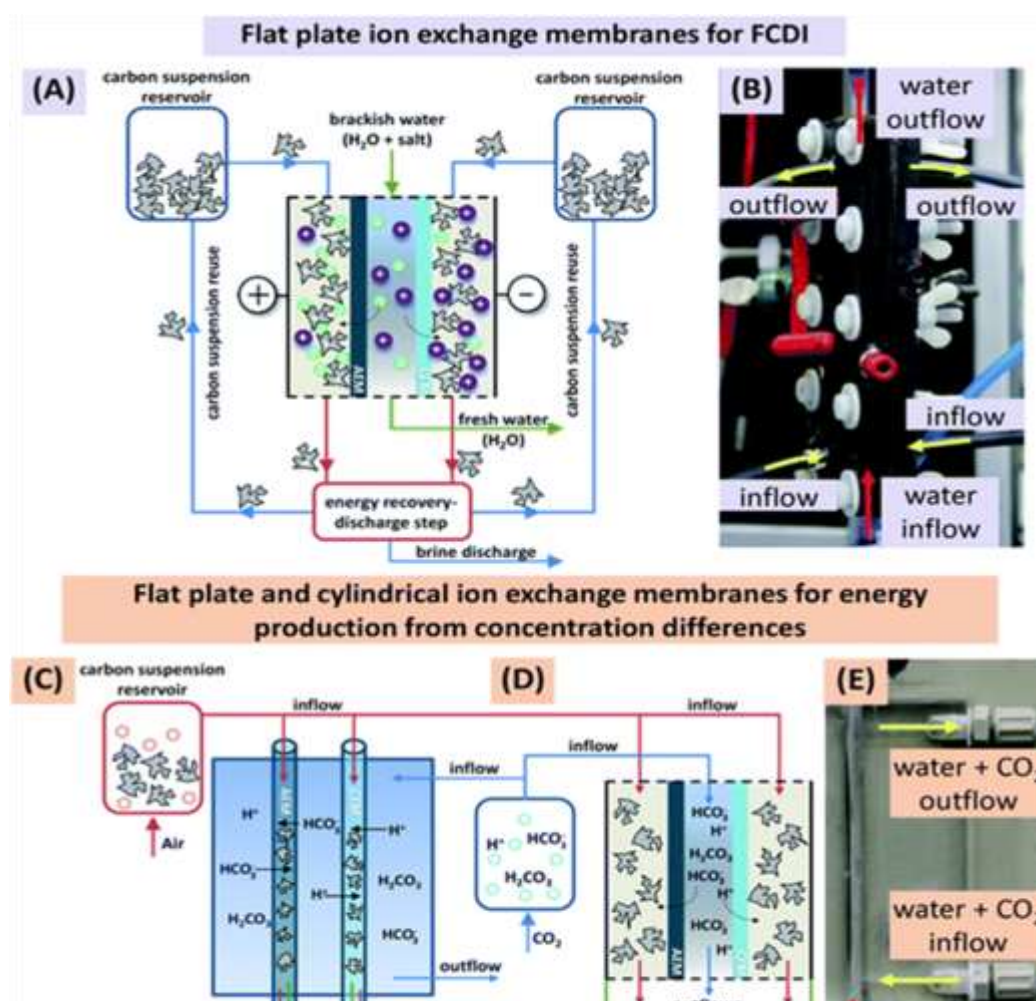


Fig. 8: A) Schematic diagram of continuous FCDI operation and (B) a photograph of the cell. Schematic diagrams of (C) tubular and (D) flat plate IEMs used for energy recovery. (E) A photograph of the tubular cell design [31]

Other ground-breaking design is by Cho et al. [56] utilised a “honeycomb-shaped” structure for a compact and scalable 3D FCDI, which could be used in a repetitive manner for upscaling. As illustrated in Figure 9, the insides of the channels were coated with IEM and a graphene layer (functioning as current collector). The porous structure provides structural support as well as a path for ion transfer.

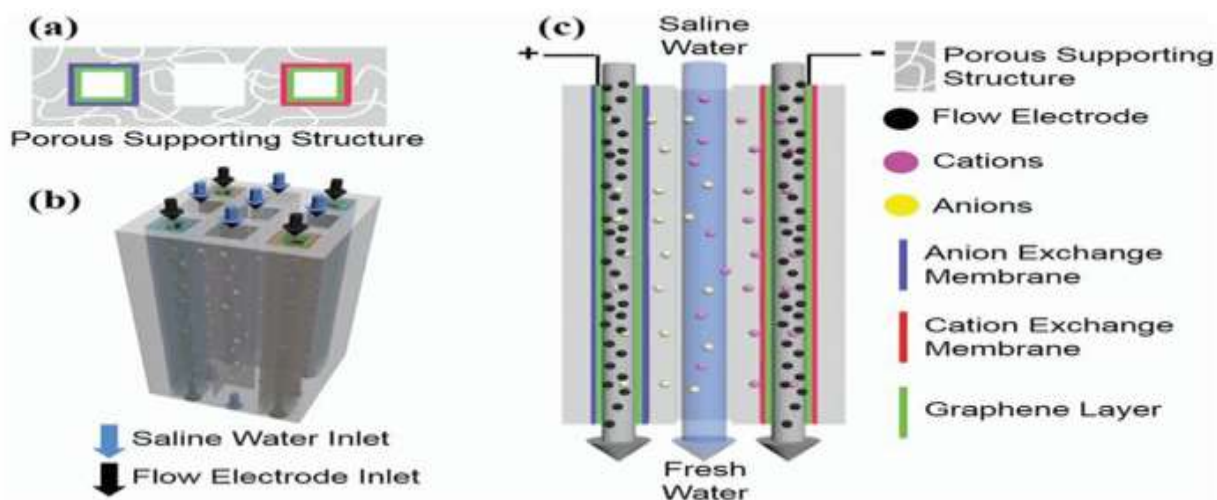


Fig. 9: Three-dimensional honeycomb-shaped FCDI cell: (a) top-view (1×3 channel cell), (b) 3×3 -channel cell, and (c) desalination process [56]

The 3D FCDI system eliminates the need for a spacer, free-standing IEMs, and bulky current collectors, resulting in a significantly more compact and space-efficient cell design compared to conventional FCDI configurations. While the system is impressively scalable, the observed current density was lower than in conventional FCDI cells, but the desalination efficiency has increased threefold [56]. Moreover, the unit cell lends itself well to 3D scaling, with both desalination efficiency and capacity improving markedly as cell size or the number of units increases [57]. This innovative design has stimulated further exploration into advanced FCDI cell architectures.

5.2 Current Collectors

Current collectors are a core component of the FCDI module, responsible for creating the potential difference across the flow electrodes. Their material properties and dimensions play a critical role in facilitating charge transport by influencing the system’s electrical resistance [19].

Ideal current collectors should exhibit high electrical conductivity, mechanical robustness, low weight, and cost-effectiveness. Additionally, they should be readily machinable, available, and offer excellent corrosion resistance within the operating voltage range of the FCDI cell [27].

In early FCDI studies [11,13], including the pioneering work by Jeon et al., stainless steel was commonly used for current collectors, often designed with carved, serpentine flow channels. However, stainless steel suffers from corrosion, particularly at the anode during the treatment of chloride-containing solutions. Consequently, graphite plates have become the preferred current collector material in subsequent research due to their superior corrosion resistance and overall stability such environments [29,58].

Porada et al. [31] used titanium wires and platinum plates as current collectors, but another innovative design was reported last year by Zhang et. al. [59] where 3D titanium mesh, illustrated in Figure 10, was used as current collector in FCDI for salt separation and enrichment. This new approach substantially enhanced the charge transfer process and exhibited exceptional cyclic stability over 100 desalination cycles. Other reported current collector materials include gold-plated copper [60] and epoxy-impregnated graphite plates [61].

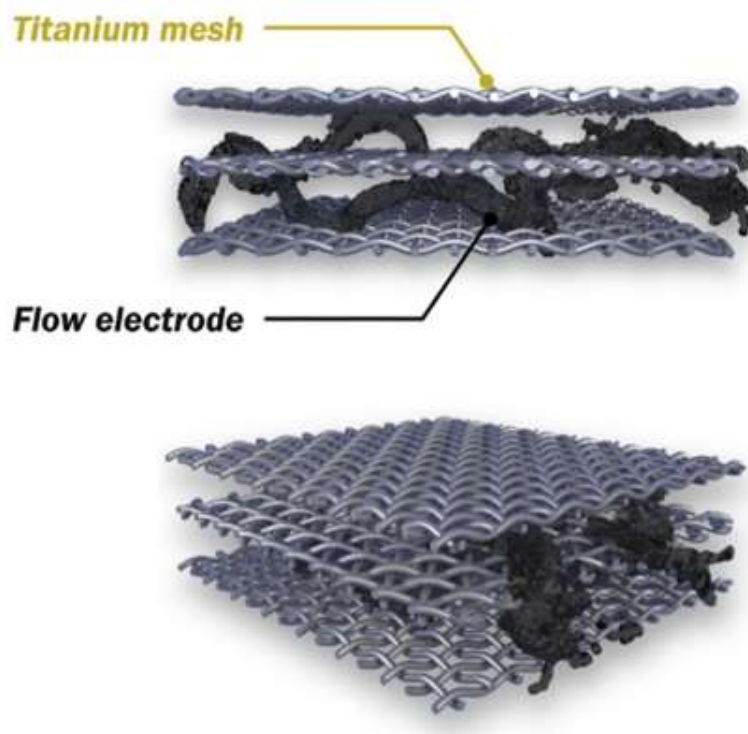


Fig. 10: Three-dimensional titanium mesh current collectors [59].

5.3 Flow Channels

The design of flow channel geometry, including the configuration of inlets, outlets, and the distribution of streams within the cell compartments, differs across studies. The geometry of the channels engraved on the surface influences the contact area, which significantly impacts ion transport. Moreover, it affects the system's energy consumption, largely governed by the rheological behaviour of the carbon slurry [19].

Typically, these channels are carved on a single side of the current collector. However, graphite collectors with channels etched on both sides have also demonstrated effectiveness in stacked FCDI cell configurations [19]. A recent innovative approach is Yang et al.'s [62] use of titanium meshes instead of the bulky current collectors. This modification reduces the charge transport distance and enhances ion adsorption onto the carbon particles.

5.4 Separating Material

The separator plays a pivotal role by preventing the mixing of the flowing carbon particles with the feed water, while permitting selective ion transport to and from the electrode channels. It also serves as a barrier against the intrusion of foulants into the flow electrode solution. Nevertheless, separator fouling remains a potential challenge in the operation of FCDI systems.

In most FCDI cell architectures, IEMs are employed as separators [63]. IEMs originally developed for ED applications, such as Neosepta membranes from Astom Corporation and fumasep membranes from Fumatech BWT GmbH, have been widely used in FCDI studies [11,13,29,31].

Yang et al. showed that IEMs with low electrical resistance and high exchange capacity are essential for facilitating effective charge transfer, thus improving the overall desalination efficiency in FCDI systems [64]. Notably, a recent study reported that performance deterioration due to IEM fouling was minimal, attributing this to the inherently low fouling tendency of the membrane [65].

To simplify the FCDI system and reduce material costs, Lee et al. developed a hybrid structure in which IEMs were coated directly onto a porous ceramic spacer, effectively combining the membrane and the spacer. This innovation eliminated the need for costly free-standing IEMs [66].

Beyond the conventional use of IEMs, alternative separators have also been explored. Nativ et al. [67] proposed the use of NF membranes in FCDI cells to achieve selective separation between monovalent and divalent ions. Hatzell et al. [58] proposed a configuration utilizing a porous separator, representing a promising direction for developing low-cost FCDI systems [63].

5.5 Spacer and Endplates

The spacer, which channels the flow of water between the separating materials, influences FCDI's performance by determining the hydraulic retention time. Materials commonly used for spacers include nylon [68] and polyester [32], owing to their mechanical stability and chemical resistance. In addition, various alternative materials have been explored, such as mesh spacers, polymeric flannel spacers, and shaped silicone gaskets, each tailored to fit specific FCDI cell architectures [11,13,29,31]. Cho et al. [56] utilised a cordierite spacer to prolong the residence time of saline water, thereby improving ion removal efficiency. Additionally, coating a porous spacer with CEM and AEM has been proposed as a cheaper alternative to standalone IEMs [66].

Although endplates do not directly influence the performance of FCDI systems, they play a role in ensuring the structural integrity and longevity of the module [19]. The complex design and stringent sealing requirements of FCDI units contribute to elevated operational costs [69]. To balance durability and affordability, materials such as polyvinyl chloride, polycarbonate, and acrylic are commonly employed [70].

Researchers explored innovative ways to improve the performance and broaden the range of applications of FCDI [19]. The following section presents the diverse modes of FCDI configuration.

6 Operating Configuration

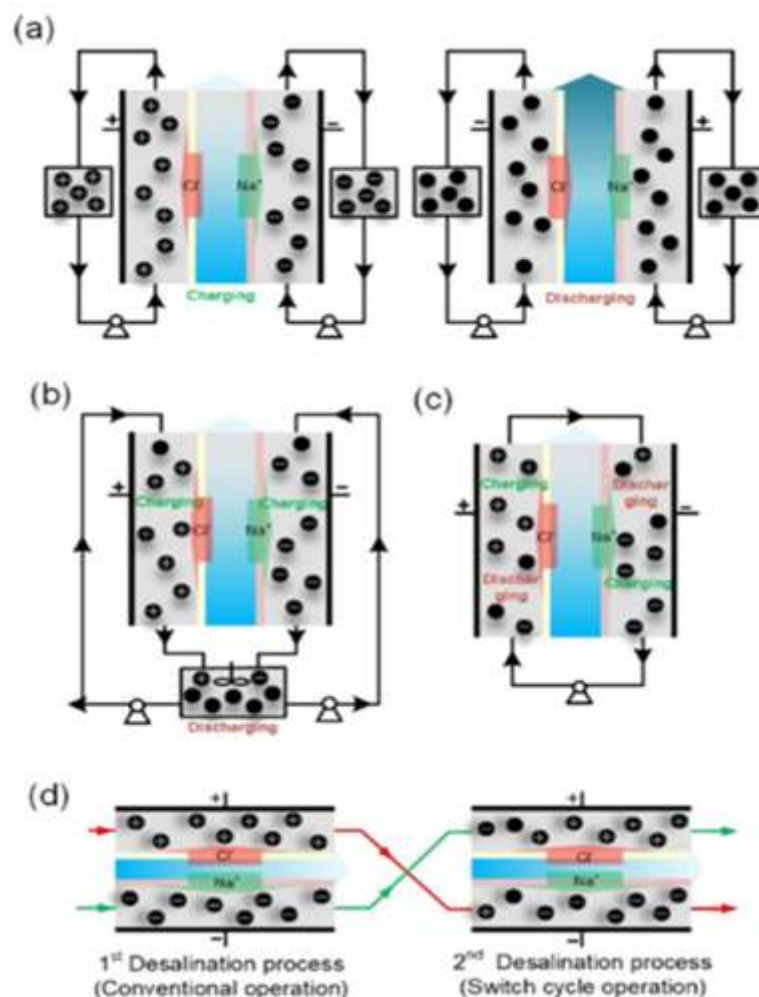
The operational mode has a considerable influence on the FCDI system's desalination performance. Studies on FCDI operation are mainly classified into two categories: single- and multi-module configurations. In single-module setups, the flow electrodes circulate within a single unit, whereas in multi-module configurations, electrodes flow across multiple modules to enable continuous desalination [54].

6.1 Single Module Configuration

In open-cycle operation with continuously refreshed flow electrodes, the system can theoretically achieve infinite ion adsorption capacity. However, the high operating costs of maintaining a constant supply of fresh flow electrodes render this approach economically infeasible in most practical applications [57]. Therefore, closed-cycle operation modes are used in practical FCDI operation. Two types of closed-cycle operation are the Isolated Closed-Cycle (ICC) mode and Short-Circuited Closed-Cycle (SCC) mode, illustrated in Figure 11, different depending on whether the flow electrodes are mixed or not.

In ICC mode, the cathode and anode flow electrodes are directed into two different reservoirs following the adsorption process. Electrosorption and desorption occur sequentially, resembling the batch mode of traditional CDI systems [51]. Initially, conductivity decreases rapidly as ions are adsorbed, but it soon increases again due to electrode saturation and the limited availability of active adsorption sites, characteristic of fixed electrode systems [7].

In contrast, in SCC mode, the cathode and anode flow-electrodes are mixed in a single reservoir. This shared recirculation facilitates faster ion release and regeneration, improving ion removal and reducing energy demand compared to ICC [51].



leveraging gravity to extend their residence time. Because the particles settle faster than the continuous water phase flows, their concentration within the module increases, enhancing performance. Meanwhile, the overall carbon concentration in the system, including tubing, remains lower, which eases pumping requirements.

In 2016, Yang et al. [70] introduced the first FCDI stack design, which was developed by simply stacking individual FCDI cells, each incorporating a single pair of IEMs. This configuration enabled compact cell integration and enhanced scalability.

6.2 Multi-module Configuration

Jeon et al. [73] introduced an innovative FCDI operation mode called the switch cycle mode, where the charged cathode and anode flow electrodes of the first module are rerouted to the opposite channels of a second module. This setup achieved improved desalination performance over the SCC mode.

Moreover, by altering the position of the IEMs in the second module, the system can be transformed into a new configuration known as continuous cycle mode, wherein the effluent from the first module corresponds to desalinated water and that from the second module represents the concentrated brine stream [57].

7 Flow Electrode

Flow electrodes are fundamental to achieving continuous operation in FCDI systems. They consist of charged carbon particles suspended in an electrolyte [31]. To optimise process stability, energy efficiency, and the quality of the treated water, it is crucial to understand how electrode properties influence FCDI operational parameters [74]. Given their central role, considerable research has focused on enhancing both the carbon materials and the electrolyte composition that constitute the flow electrodes.

7.1 Carbon-based Materials

Activated Carbon (AC) was predominantly employed in early FCDI studies [8,11,13] as the active material for preparing flow-electrode suspensions. AC is considered highly suitable due to its favourable electrochemical characteristics, including high surface area, low cost, and ease of processing [74]. In FCDI systems, the effectiveness of ion separation is largely determined by critical characteristics of the AC electrodes, including particle size, pore volume, surface area, and surface functional groups [32].

Rommerskirchen et al. [75] demonstrated that the presence of mesopores in AC improves desalination performance by facilitating ion transport compared to predominantly microporous structures. Most commonly used AC materials in FCDI have specific surface areas in the range of 1000-1500 m²/g. Although high surface area generally correlates with improved ion adsorption capacity, material selection is also driven by cost, particle morphology, and size distribution [15].

The electrical conductivity of the flow-electrode is highly dependent on the carbon mass loading (wt%) in the flow-electrode suspension [15]. Initially, flow electrodes were formulated with low carbon content so as to be less viscous and more pumpable. However, Porada et al. [31] later showed that increasing AC content significantly enhances desalination performance due to improved electrical conductivity and charge transport. Despite these benefits, higher AC concentrations result in elevated suspension viscosity, thereby increasing the required pumping energy. This trade-off relationship of improved salt removal versus energy efficiency constrains the practical carbon loading to below 20 wt%, beyond which the risk of clogging and flow issues becomes significant due to the physical nature of the carbon particles [32].

Consequently, two main targets have emerged to develop optimum AC electrodes for FCDI operation: 1) maximising loading capacity to enhance salt adsorption, while 2) minimising viscosity to reduce pumping energy and operational complications. Simultaneously achieving both objectives remains a significant challenge. Therefore, recent research has focused on optimising charge percolation and exploring alternative carbon materials, non-carbon

additives, and surface treatments. Hatzell et al. [9] presented a comprehensive review on materials used in flow-electrodes.

Hatzell et al. [76] modified AC using nitric acid to introduce oxygen-containing surface functional groups. This chemical oxidation process was found to reduce the viscosity of carbon suspensions, thereby enabling higher carbon mass loadings while maintaining pumpability.

Similarly, Park et al. [32] developed and evaluated surface-modified AC suspensions incorporating ion-selective functional groups. Their aim was to achieve greater carbon loadings without compromising the flowability of the suspension.

To further enhance FCDI performance, Xu et al. [77] proposed an asymmetric FCDI configuration using an AC/manganese-dioxide suspension as the anodic flow electrode, and a conventional AC suspension as the cathodic one. This system successfully expanded the operational voltage window to 1.8 V, significantly improving salt removal efficiency compared to traditional symmetric FCDI cells.

Chang et al. [74] also explored asymmetric FCDI systems, using activated carbon at the anode and copper hexacyanoferrate at the cathode. This combination also enabled operation at higher voltages and improved ion removal performance. However, the system exhibited a greater pH shift in the concentrate stream compared to conventional symmetric systems, posing potential challenges for downstream applications.

All these studies share a common conclusion: the properties and composition of flow-electrode materials are critical determinants of FCDI performance. The research to date has laid a strong foundation and provided an essential set of strategies for tailoring flow-electrode materials. Importantly, the selection of the optimal flow electrode may vary depending on the target application.

7.2 Electrolyte Concentration and Composition

In a deionized water solution with a typical electrolyte such as NaCl, the solution itself exhibits relatively low electrical resistance. However, the introduction of AC to the electrolyte creates a non-homogeneous mixture, resulting in a moderate yet non-negligible electrical conductivity ranging from approximately 0.1 to 1 mS/cm [78]. Within the FCDI system, when the flow electrodes come into contact with the current collector, electrons are transferred to the carbon particles. Despite this mechanism, the overall flow-electrode's electrical conductivity is generally lower than that of static electrodes in conventional CDI systems [15]. This reduced conductivity in FCDI poses a limitation: charge transport is primarily hindered by the relatively high internal electrical resistance of the flow-electrodes, which constrains the desalination and energy efficiency of the process.

To address this limitation without resorting to increasing the carbon loading, two alternative strategies have been explored [33]: 1) increasing the electrolyte salinity, which can reduce the internal resistance within the flow electrode suspension by enhancing ionic conductivity; in addition to 2) adding supplementary charged species, such as conductive additives or redox-active agents, to facilitate charge transfer and percolation efficiency.

Yang et al. [33] employed high salt concentration electrolyte and confirmed its effectiveness in reducing the internal resistance of the electrode and improving desalination efficiency. However, it can lead to undesired ion diffusion into the feed water, compromising product quality. Therefore, optimisation is essential to balance desalination efficiency with minimal reverse ion diffusion [10].

Another strategy to improve the conductivity of the flow-electrode is the introduction of conductive additives, which could be of two: (i) highly conductive solids, or (ii) aqueous electron-mediators.

Liang et al. [79] incorporated carbon black into AC-based flow electrodes. Despite its relatively low specific surface area ($<120 \text{ m}^2/\text{g}$), carbon black significantly enhanced desalination and charge transport by lowering the internal resistance of the FCDI system. Surprisingly, this additive also reduced the system's energy consumption and enabled a broader voltage operation window.

Yang et al. [64] evaluated graphite powder and demonstrated that its particle size, shape, conductivity, and pore structure influence FCDI performance. The authors concluded that plate-shaped graphite particles showed improved conductivity without clogging issues and attributed this observation to the particles' alignment with the direction of flow and its larger size.

Both Cho et al. [80] and Tang et al. [81] demonstrated excellent electrochemical properties when adding carbon nanotubes to the flow-electrode, due to their hollow tubular structure and interconnected nanoscale network. Just 0.25 wt% carbon nanotubes addition enhanced the electrical connectivity leading to double the salt removal rate. However, carbon nanotubes tend to agglomerate due to strong van der Waals forces and poor hydrophilic properties [57].

Graphene and reduced graphene oxide have also proven effective. Li et al. [82] reported that these additives improve electron transport and dispersion of carbon particles, contributing to enhanced salt removal efficiency.

Nonetheless, while solid additives can significantly improve conductivity, they pose a risk of aggregation and clogging, especially at high loadings [19]. Beyond solid additives, electrolyte pH control has also been proven beneficial, particularly that pH fluctuations caused by minor Faradaic reactions can impair desalination efficiency [33]. Nativ et al. [48] mitigated this by introducing acid and base to neutralise the pH in the anodic and cathodic flow-electrodes, thereby enhancing the salt adsorption capacity.

Electron mediators represent another approach to improve charge transport. These additives function via fast, reversible redox reactions.

Hatzell et al. [8] found that p-phenylenediamine significantly increased the capacitance and reduced ohmic resistance compared to unmodified carbon slurries. Similarly, Ma et al. [83] incorporated hydroquinone, enabling rapid redox cycling with benzoquinone. This approach significantly boosted both ion adsorption and desorption rates.

However, the addition of chemical mediators must be approached cautiously. Since ion migration across the membrane is governed by chemical potential gradients, there is a risk of chemical transfer into the product stream. Preventing the introduction of toxins into the effluent water necessitates careful selection and monitoring of conductive additives [10].

7.3 Regeneration

The flowability of the flow-electrode enables regenerating the carbon material elsewhere outside the main cell, allowing for a wide range of configurations. The earliest FCDI experiments employed simple single-pass operation modes for both the saline feed and the flow electrodes [13]. In these initial studies, regeneration was implemented in batch-like charge-discharge cycles [29], through a separate regeneration module [11], a dedicated tank [19], or via an external treatment step [58]. As the technology evolved, researchers proposed novel regeneration strategies to support more efficient or continuous operation, such as 1) regeneration by mixing, 2) electrical regeneration, and 3) chemical reactivation.

The research group who reported the first FCDI publication also pioneered the concept of regeneration by mixing [29]. In this method, oppositely charged flow electrodes are combined, enabling electrical neutralisation and ion desorption. The adsorbed salt ions are released into the continuous phase, while the carbon particles are simultaneously regenerated. This approach can be sustained for extended periods as the salinity of the liquid increases gradually. This method has been widely adopted in subsequent FCDI studies because of its technical simplicity and semi-continuous operation potential [84,85].

Electrical regeneration was introduced in 2014 [11], where two FCDI cells share the flow-electrode in a circuit. One cell continuously performs desalination, while the other operates as a regeneration module, concentrating saline water and electrically discharging the flow electrodes. This approach also opened the door to

energy recovery from the flow electrodes during regeneration, a concept first investigated by the same research group that introduced FCDI [29]. They demonstrated that energy could be harvested during the discharge phase in a manner analogous to the charge-discharge cycles of conventional CDI systems. A key advantage of electrical regeneration is its operational stability, which can be challenging to achieve in systems relying on mixing-based regeneration. The latter necessitates additional operations (i.e. settling or crossflow filtration) to retain the carbon particles in the flow-electrode.

Complete charge-discharge reversibility in any of the above-mentioned regeneration methods is unachievable due to the concentration gradient between the feed and the electrolyte [86]. Maintaining performance over long-term operation requires effective regeneration and activation to restore the adsorption capacity of the carbon-based material. While thermal regeneration of spent carbon-materials is generally the most popular choice due to its simplicity, the energy demand is not called for in the case of FCDI applications. Hence, chemical reactivation, which only involves acid washing followed by neutralisation, is recommended. It is worth mentioning that this process also often enhances the surface area [87].

8 Applications beyond Desalination

While the most extensively studied application of FCDI is water desalination [27], more studies have explored FCDI for resource recovery, contaminant removal, and other emerging applications [19,27].

Linnartz et al. [88] used FCDI for salt metathesis through a double displacement reaction. Their study employed four identical FCDI cells to concentrate magnesium sulphate from dilute feed solutions. This method shows significant potential for salt recovery processes by allowing concurrent salt recombination and concentration, yielding high-value product streams.

Zhang et al. [89] developed an FCDI process targeting ammonia recovery, wherein a membrane module was submerged in the flow cathode, enabling the direct stripping of ammonia from the electrode stream. This approach facilitates the selective removal and preconcentration of ammonia, which can subsequently be recovered as ammonium salts, with potential market value as fertilizers. The same research group later presented a simplified FCDI system based on charge-discharge cycles for ammonia recovery from wastewater [90]. Similarly, Fang et al. [85] employed an SCC FCDI system for ammonia recovery, achieving favourable concentration factors using synthetic wastewater as a feed.

Beyond nutrient recovery, He et al. [91] applied FCDI in brackish water softening, again using the SCC mode. The system was shown to be cost-effective, and the continuous mixing of charged carbon particles played a critical role in inhibiting scaling on the electrode surface.

FCDI was employed for the simultaneous removal of multiple heavy metals. Researchers explored cadmium removal [92] and copper removal [93] using FCDI under continuous operation mode. Notably, the setup enabled efficient regeneration and reuse of the electrode material, highlighting FCDI's potential for sustainable and scalable treatment of metal-contaminated water.

The growing interest in FCDI in recent years reflects the technology's flexibility and promising potential. Beyond the previously discussed applications, FCDI has been explored for nutrient recovery, including nitrogen and phosphorus [94], as well as for the removal of contaminants like nitrate [68] and uranium [84].

In addition to standalone FCDI systems, hybrid configurations integrating FCDI with conventional processes, such as NF [95], have also been investigated. Similar to ED, FCDI could further concentrate RO brine [24], as a step towards achieving ZLD.

9 Commercialisation Status, Challenges, and Future Perspectives

FCDI has emerged as a promising electrically driven desalination technology, offering continuous operation, high water recovery, and unique advantages in treating high salinity streams. However, its development remains in the early stages [19]. The transition from laboratory prototypes to commercially viable systems is still hindered by a range of technical and economic challenges.

9.1 Current Status

Despite growing interest in FCDI, most reported systems remain limited to small-scale setups (less than 100 L/day) [27], with no pilot- or full-scale commercial units currently in operation [19]. This limited scale hinders accurate assessment of capital costs and long-term stability under industrial conditions, thereby delaying its market readiness [96]. While the flat systems are currently predominant [97], ongoing research is exploring alternative geometries to improve scalability and operational efficiency [56]. Nonetheless, system durability remains a concern, especially due to carbon particle clogging within the flow channels. CFD simulations have proven valuable in designing flow paths and reducing dead zones [98,99], thereby enhancing mass transfer and operational longevity.

9.2 Economic and Energy Perspectives

Regarding FCDI's total capital costs, more than 50% is attributed to the high cost of IEMs [100], which is a primary barrier to FCDI deployment. This encouraged researchers to use other more cost-efficient types of separators as discussed above [63]. Similarly, current collectors and flow-electrodes remain costly but could be improved by better design and material selection [101]. Pumping costs contribute to most operating costs [102], while the pretreatment requirements to mitigate fouling and scaling further increase the economic burden [27]. Despite these challenges, the modularity of FCDI systems and potential for diverse applications could enhance economic feasibility [19].

Regarding FCDI's energy efficiency, it is substantially better than conventional CDI [72]. This is largely attributed to the pseudo steady-state operation of FCDI, enabled by continuous electrode regeneration [27]. Furthermore, 36% of energy stored in the charged electrodes was successfully recovered before regeneration, further improving system efficiency [103].

Nevertheless, a key disadvantage lies in the high pumping energy required for electrode slurry recirculation, contributing to as high as 60% of the total electrical energy [27]. Optimising system-level operation to balance electrical and hydraulic energy demands is crucial for achieving overall efficiency.

Importantly, FCDI operates at low voltages (~ 1.2 V), making it suitable for integration with off-grid renewable energy sources. Pilot-scale CDI systems powered by photovoltaics have already demonstrated continuous desalination, suggesting a viable pathway for future FCDI deployments in remote or decentralised contexts [104].

9.3 Operational Challenges

While FCDI can achieve high water recovery (up to 97%) [103], this performance can be compromised by water transport through IEMs diluting the brine, which is the challenge faced by electrodialysis [27]. Another common challenge is the fouling and scaling of membranes, which reduce system performance, elevate energy demands, and shorten lifespan, particularly when treating complex feedwaters [27]. Although pretreatment and cleaning protocols are effective, they add cost and maintenance burdens.

9.4 Future Outlook and Research Needs

To accelerate the commercialisation of FCDI, several key research directions must be prioritised. One critical area is cell design and system optimisation. Novel architectural designs and assemblies can improve modularity and scalability while reducing component bulk.

Equally important is the development of advanced materials. Innovations such as profiled or composite IEMs and charge-transfer flow-electrodes offer the potential to enhance ion selectivity, reduce energy consumption, and ultimately lower capital costs.

Another promising pathway lies in system modelling. Comprehensive and experimentally validated models capturing both capacitive and electrodialytic mechanisms are needed to predict and optimise performance under varying operational conditions.

Despite FCDI's clear potential as a brine concentrator, its integration with RO is overlooked. FCDI–RO hybrid systems for ZLD remains a major research gap, with only one study to date [105]. Their potential for energy-efficient, high-recovery desalination warrants focused attention.

In parallel, application targeting can significantly strengthen the case for FCDI commercialisation. Niche markets that require selective ion removal or resource recovery, such as phosphate, lithium, or ammonia extraction, offer opportunities where FCDI may outperform conventional technologies, both technically and economically.

Finally, industry–academia collaboration is essential. Robust partnerships can support prototype validation, reduce production costs through economies of scale, and facilitate the customisation of systems to meet specific industrial or municipal requirements.

10 Conclusion

Flow Capacitive Deionization (FCDI) is emerging as a promising electrically driven technology. Its unique ability to operate continuously, tolerate high salinities, and achieve high water recovery at relatively low specific energy consumption positions it as a compelling candidate for advanced brine management and Zero Liquid Discharge (ZLD) strategies.

Yet, despite these advantages, the pathway to commercial deployment remains hindered by technical, economic, and scalability challenges. In particular, the integration of FCDI with reverse osmosis for complete ZLD has not been adequately explored, representing a critical opportunity for future research. Continued progress in materials development, system modelling, targeted applications, and collaborative scale-up efforts will be essential to unlock FCDI's full potential and position it as a viable solution for next-generation desalination and resource recovery.

References

- [1] AlMarzooqi FA, Al Ghaferi AA, Saadat I, Hilal N (2014) Application of Capacitive Deionisation in water desalination: A review. *Desalination* 342:3-15
- [2] Porada S, Zhao R, Van Der Wal A, Presser V, Biesheuvel PM (2013) Review on the science and technology of water desalination by capacitive deionization. *Prog Mater Sci* 58:1388-1442
- [3] Lee JB, Park KK, Eum HM, Lee CW (2006) Desalination of a thermal power plant wastewater by membrane capacitive deionization. *Desalination* 196:125-134
- [4] Folaranmi G, Bechelany M, Sifat P, Cretin M, Zavisla F (2020) Towards Electrochemical Water Desalination Techniques: A Review on Capacitive Deionization, Membrane Capacitive Deionization and Flow Capacitive Deionization. *Membranes* 10:96
- [5] Xing W, Liang J, Tang W, He D, Yan M, Wang X, Luo Y, Tang N, Huang M (2020) Versatile applications of capacitive deionization (CDI)-based technologies. *Desalination* 482:114390
- [6] Chen L, Yin X, Zhu L, Qiu Y (2018) Energy recovery and electrode regeneration under different charge/discharge conditions in membrane capacitive deionization. *Desalination* 439:93-101
- [7] Chai S, Xi J, Chen L, He W, Shen J, Gong H (2022) Selective Ion Removal by Capacitive Deionization (CDI)-Based Technologies. *Processes* 10:1075

- [8] Hatzell KB, Beidaghi M, Campos JW, Dennison CR, Kumbur EC, Gogotsi Y (2013) A high performance pseudocapacitive suspension electrode for the electrochemical flow capacitor. *Electrochim Acta* 111:888-897
- [9] Hatzell KB, Boota M, Gogotsi Y (2015) Materials for suspension (semi-solid) electrodes for energy and water technologies. *Chem Soc Rev* 44:8664-8687
- [10] Shin YU, Lim J, Boo C, Hong S (2021) Improving the feasibility and applicability of flow-electrode capacitive deionization (FCDI): Review of process optimization and energy efficiency. *Desalination* 502:114930
- [11] Gendel Y, Rommerskirchen AKE, David O, Wessling M (2014) Batch mode and continuous desalination of water using flowing carbon deionization (FCDI) technology. *Electrochem commun* 46:152-156
- [12] Shanbhag S, Whitacre JF, Mauter MS (2016) The Origins of Low Efficiency in Electrochemical De-Ionization Systems. *J Electrochem Soc* 163:E363-E371
- [13] Jeon S Il, Park HR, Yeo JG, Yang S, Cho CH, Han MH, Kim DK (2013) Desalination via a new membrane capacitive deionization process utilizing flow-electrodes. *Energy Environ Sci* 6:1471-1475
- [14] Rommerskirchen A, Gendel Y, Wessling M (2015) Single module flow-electrode capacitive deionization for continuous water desalination. *Electrochem commun* 60:34-37
- [15] Doornbusch GJ, Dykstra JE, Biesheuvel PM, Suss ME (2016) Fluidized bed electrodes with high carbon loading for water desalination by capacitive deionization. *J Mater Chem A Mater* 4:3642-3647
- [16] Blair JW, Murphy GW (1960) Electrochemical Demineralization of Water with Porous Electrodes of Large Surface Area. 206-223
- [17] Johnson AM, Newman J (1971) Desalting by Means of Porous Carbon Electrodes. *J Electrochem Soc* 118:510-517
- [18] Farmer JC, Richardson JH, Fix D V. (1996) Desalination with Carbon Aerogel Electrodes. 298:
- [19] Tauk M, Sistat P, Habchi R, Cretin M, Zaviska F, Bechelany M (2025) Exploring flow-electrode capacitive deionization: An overview and new insights. *Desalination* 597:118392
- [20] Tran NAT, Khoi TM, Phuoc NM, Jung H Bin, Cho Y (2022) A review of recent advances in electrode materials and applications for flow-electrode desalination systems. *Desalination* 541:116037
- [21] Yu F, Yang Z, Cheng Y, Xing S, Wang Y, Ma J (2022) A comprehensive review on flow-electrode capacitive deionization: Design, active material and environmental application. *Sep Purif Technol* 281:119870
- [22] Ma J, Chen L, Yu F (2024) Environmental applications and perspectives of flow electrode capacitive deionization (FCDI). *Sep Purif Technol* 335:126095
- [23] Tauk M, Bechelany M, Sistat P, Habchi R, Cretin M, Zaviska F (2024) Ion-selectivity advancements in capacitive deionization: A comprehensive review. *Desalination* 572:117146
- [24] Rommerskirchen A, Linnartz CJ, Egidi F, Kendir S, Wessling M (2020) Flow-electrode capacitive deionization enables continuous and energy-efficient brine concentration. *Desalination* 490:114453
- [25] Rommerskirchen A, Kalde A, Linnartz CJ, Bongers L, Linz G, Wessling M (2019) Unraveling charge transport in carbon flow-electrodes: Performance prediction for desalination applications. *Carbon N Y* 145:507-520
- [26] Ma J, Zhai C, Yu F (2023) Review of flow electrode capacitive deionization technology: Research progress and future challenges. *Desalination* 564:116701
- [27] Zhang C, Ma J, Wu L, Sun J, Wang L, Li T, Waite TD (2021) Flow Electrode Capacitive Deionization (FCDI): Recent Developments, Environmental Applications, and Future Perspectives. *Environ Sci Technol* 55:4243-4267
- [28] Liu Z, Shang X, Li H, Liu Y, Liu Z, Shang X, Li H, Liu Y (2021) A Brief Review on High-Performance Capacitive Deionization Enabled by Intercalation Electrodes. *Global Challenges* 5:2000054
- [29] Jeon S Il, Yeo JG, Yang S, Choi J, Kim DK (2014) Ion storage and energy recovery of a flow-electrode capacitive deionization process. *J Mater Chem A Mater* 2:6378-6383
- [30] Choi J, Dorji P, Shon HK, Hong S (2019) Applications of capacitive deionization: Desalination, softening, selective removal, and energy efficiency. *Desalination* 449:118-130
- [31] Porada S, Weingarth D, Hamelers HVM, Bryjak M, Presser V, Biesheuvel PM (2014) Carbon flow electrodes for continuous operation of capacitive deionization and capacitive mixing energy generation. *J Mater Chem A Mater* 2:9313-9321

- [32] Park HR, Choi J, Yang S, Kwak SJ, Jeon S Il, Han MH, Kim DK (2016) Surface-modified spherical activated carbon for high carbon loading and its desalting performance in flow-electrode capacitive deionization. *RSC Adv* 6:69720-69727
- [33] Yang S, Choi J, Yeo JG, Jeon S Il, Park HR, Kim DK (2016) Flow-Electrode Capacitive Deionization Using an Aqueous Electrolyte with a High Salt Concentration. *Environ Sci Technol* 50:5892-5899
- [34] Chung HJ, Kim J, Kim DI, Gwak G, Hong S (2020) Feasibility study of reverse osmosis-flow capacitive deionization (RO-FCDI) for energy-efficient desalination using seawater as the flow-electrode aqueous electrolyte. *Desalination* 479:114326
- [35] Adewole JK, Al Maawali HM, Jafary T, Firouzi A, Oladipo H (2022) A review of seawater desalination with membrane distillation: material development and energy requirements. *Water Supply* 22:8500-8526
- [36] Liu E, Lee LY, Ong SL, Ng HY (2020) Treatment of industrial brine using capacitive deionization (CDI) towards zero liquid discharge - challenges and optimization. *Water Res* 183:116059
- [37] Gu H, Hou C, Mao Y, Wu D (2025) Navigating the Dual Pathways of Ion Removal in Flow-Electrode Capacitive Deionization: Capacitive Trapping vs. Electrodialytic Migration. <https://doi.org/10.2139/SSRN.5217000>
- [38] Johnson DJ, Hilal N (2021) Can graphene and graphene oxide materials revolutionise desalination processes? *Desalination* 500:114852
- [39] Miao L, Gao M, Xiao W, Kang Y, Li R, Kong H, Mou H, Chen W, Ao T (2024) Progress toward adsorption mechanism exploration method for capacitive deionization: Experimental, mathematical model, computational chemistry and machine learning. *Desalination* 586:117850
- [40] Rommerskirchen A, Alders M, Wiesner F, Linnartz CJ, Kalde A, Wessling M (2020) Process model for high salinity flow-electrode capacitive deionization processes with ion-exchange membranes. *J Memb Sci* 616:118614
- [41] Papastavrou G (2010) Combining electrochemistry and direct force measurements: From the control of surface properties towards applications. *Colloid Polym Sci* 288:1201-1214
- [42] Shi M, Jia H, Liu J, Gao M, Wang C, Wang F, Xia M, Jin W, Tong G (2025) Engineering sustainable porous carbon electrodes for practical-level capacitive deionization desalination. *Coord Chem Rev* 543:216949
- [43] Huang Q, Sheng L, Wu T, Huang L, Yan J, Li M, Chen Z, Zhang H (2025) Research progress on the application of carbon-based composites in capacitive deionization technology. *Desalination* 593:118197
- [44] Biesheuvel PM, Fu Y, Bazant MZ (2011) Diffuse charge and Faradaic reactions in porous electrodes. *Phys Rev E Stat Nonlin Soft Matter Phys* 83:061507
- [45] Biesheuvel PM, Fu Y, Bazant MZ (2012) Electrochemistry and capacitive charging of porous electrodes in asymmetric multicomponent electrolytes. *Russian Journal of Electrochemistry* 48:580-592
- [46] Zhang C, He D, Ma J, Tang W, Waite TD (2018) Faradaic reactions in capacitive deionization (CDI) - problems and possibilities: A review. *Water Res* 128:314-330
- [47] Dykstra JE, Keesman KJ, Biesheuvel PM, van der Wal A (2017) Theory of pH changes in water desalination by capacitive deionization. *Water Res* 119:178-186
- [48] Nativ P, Badash Y, Gendel Y (2017) New insights into the mechanism of flow-electrode capacitive deionization. *Electrochem commun* 76:24-28
- [49] Elisadiki J, King'ondeu CK (2020) Performance of ion intercalation materials in capacitive deionization/electrochemical deionization: A review. *Journal of Electroanalytical Chemistry* 878:114588
- [50] Presser V, Dennison CR, Campos J, Knehr KW, Kumbur EC, Gogotsi Y (2012) The electrochemical flow capacitor: A new concept for rapid energy storage and recovery. *Adv Energy Mater* 2:895-902
- [51] Yang F, He Y, Rosentsvit L, Suss ME, Zhang X, Gao T, Liang P (2021) Flow-electrode capacitive deionization: A review and new perspectives. *Water Res* 200:117222
- [52] Farmer JC, Richardson JH, Fix D V. (1996) Desalination with Carbon Aerogel Electrodes. 298:
- [53] Tang K, Zhou K (2020) Water Desalination by Flow-Electrode Capacitive Deionization in Overlimiting Current Regimes. *Environ Sci Technol* 54:5853-5863
- [54] Jia B, Zhang W (2016) Preparation and Application of Electrodes in Capacitive Deionization (CDI): a State-of-Art Review. *Nanoscale Res Lett* 11:1-25

- [55] Lee JH, Bae WS, Choi JH (2010) Electrode reactions and adsorption/desorption performance related to the applied potential in a capacitive deionization process. *Desalination* 258:159-163
- [56] Cho Y, Lee KS, Yang SC, Choi J, Park HR, Kim DK (2017) A novel three-dimensional desalination system utilizing honeycomb-shaped lattice structures for flow-electrode capacitive deionization. *Energy Environ Sci* 10:1746-1750
- [57] Yu F, Yang Z, Cheng Y, Xing S, Wang Y, Ma J (2022) A comprehensive review on flow-electrode capacitive deionization: Design, active material and environmental application. *Sep Purif Technol* 281:119870
- [58] Hatzell KB, Iwama E, Ferris A, Daffos B, Urita K, Tzedakis T, Chauvet F, Taberna PL, Gogotsi Y, Simon P (2014) Capacitive deionization concept based on suspension electrodes without ion exchange membranes. *Electrochem commun* 43:18-21
- [59] Zhang X, Pang M, Wei Y, Liu F, Zhang H, Zhou H (2024) Three-dimensional titanium mesh-based flow electrode capacitive deionization for salt separation and enrichment in high salinity water. *Water Res* 251:121147
- [60] Moreno D, Hatzell MC (2018) Influence of Feed-Electrode Concentration Differences in Flow-Electrode Systems for Capacitive Deionization. *Ind Eng Chem Res* 57:8802-8809
- [61] Köller N, Perrey M, Brückner LK, Schäfer P, Werner S, Linnartz CJ, Wessling M (2024) Comparison of current collector architectures for Flow-electrode Capacitive Deionization. *Desalination* 582:117595
- [62] Yang F, Ma J, Zhang X, Huang X, Liang P (2019) Decreased charge transport distance by titanium mesh-membrane assembly for flow-electrode capacitive deionization with high desalination performance. *Water Res* 164:114904
- [63] Tang W, Liang J, He D, Gong J, Tang L, Liu Z, Wang D, Zeng G (2019) Various cell architectures of capacitive deionization: Recent advances and future trends. *Water Res* 150:225-251
- [64] Yang S, Park H, Yoo J, Kim H, Choi J, Han MH, Kim DK (2017) Plate-Shaped Graphite for Improved Performance of Flow-Electrode Capacitive Deionization. *J Electrochem Soc* 164:E480-E488
- [65] Hassanvand A, Chen GQ, Webley PA, Kentish SE (2019) An investigation of the impact of fouling agents in capacitive and membrane capacitive deionisation. *Desalination* 457:96-102
- [66] Lee KS, Cho Y, Choo KY, Yang SC, Han MH, Kim DK (2018) Membrane-spacer assembly for flow-electrode capacitive deionization. *Appl Surf Sci* 433:437-442
- [67] Nativ P, Lahav O, Gendel Y (2018) Separation of divalent and monovalent ions using flow-electrode capacitive deionization with nanofiltration membranes. *Desalination* 425:123-129
- [68] Song J, Ma J, Zhang C, He C, Waite TD (2019) Implication of non-electrostatic contribution to deionization in flow-electrode CDI: Case study of nitrate removal from contaminated source waters. *Front Chem* 7:422134
- [69] Cheng Y, Shi J, Zhang Q, Fang C, Chen J, Li F (2022) Recent Progresses in Adsorption Mechanism, Architectures, Electrode Materials and Applications for Advanced Electrosorption System: A Review. *Polymers* 14:2985
- [70] Yang S, Jeon S Il, Kim H, Choi J, Yeo JG, Park HR, Kim DK (2016) Stack Design and Operation for Scaling Up the Capacity of Flow-Electrode Capacitive Deionization Technology. *ACS Sustain Chem Eng* 4:4174-4180
- [71] Ma J, Zhang C, Yang F, Zhang X, Suss ME, Huang X, Liang P (2020) Carbon Black Flow Electrode Enhanced Electrochemical Desalination Using Single-Cycle Operation. *Environ Sci Technol* 54:1177-1185
- [72] Zhang C, Wu L, Ma J, Pham AN, Wang M, Waite TD (2019) Integrated Flow-Electrode Capacitive Deionization and Microfiltration System for Continuous and Energy-Efficient Brackish Water Desalination. *Environ Sci Technol*. 53(22):13364-13373
- [73] Jeon S Il, Lee J, Jo K, Kim C, Lee C, Yoon J (2019) Novel Reuse Strategy in Flow-Electrode Capacitive Deionization with Switch Cycle Operation to Enhance Desalination Performance. *Environ Sci Technol Lett* 6:739-744
- [74] Chang J, Duan F, Cao H, Tang K, Su C, Li Y (2019) Superiority of a novel flow-electrode capacitive deionization (FCDI) based on a battery material at high applied voltage. *Desalination* 468:114080
- [75] Rommerskirchen A, Kalde A, Linnartz CJ, Bongers L, Linz G, Wessling M (2019) Unraveling charge transport in carbon flow-electrodes: Performance prediction for desalination applications. *Carbon N Y* 145:507-520

- [76] Hatzell KB, Hatzell MC, Cook KM, Boota M, Housel GM, McBride A, Kumbur EC, Gogotsi Y (2015) Effect of oxidation of carbon material on suspension electrodes for flow electrode capacitive deionization. *Environ Sci Technol* 49:3040-3047
- [77] Xu X, Wang M, Liu Y, Lu T, Pan L (2017) Ultrahigh Desalination Performance of Asymmetric Flow-Electrode Capacitive Deionization Device with an Improved Operation Voltage of 1.8 v. *ACS Sustain Chem Eng* 5:189-195
- [78] Petek TJ, Hoyt NC, Savinell RF, Wainright JS (2016) Characterizing Slurry Electrodes Using Electrochemical Impedance Spectroscopy. *J Electrochem Soc* 163:A5001-A5009
- [79] Liang P, Sun X, Bian Y, Zhang H, Yang X, Jiang Y, Liu P, Huang X (2017) Optimized desalination performance of high voltage flow-electrode capacitive deionization by adding carbon black in flow-electrode. *Desalination* 420:63-69
- [80] Cho Y, Yoo CY, Lee SW, Yoon H, Lee KS, Yang SC, Kim DK (2019) Flow-electrode capacitive deionization with highly enhanced salt removal performance utilizing high-aspect ratio functionalized carbon nanotubes. *Water Res* 151:252-259
- [81] Tang K, Yiaccoumi S, Li Y, Tsouris C (2019) Enhanced Water Desalination by Increasing the Electroconductivity of Carbon Powders for High-Performance Flow-Electrode Capacitive Deionization. *ACS Sustain Chem Eng* 7:1085-1094
- [82] Li D, Ning XA, Li Y, Zhang J (2020) Nanoarchitected reduced graphene oxide composite C2N materials as flow electrodes to optimize desalination performance. *Environ Sci Nano* 7:1980-1989
- [83] Ma J, He D, Tang W, Kovalsky P, He C, Zhang C, Waite TD (2016) Development of Redox-Active Flow Electrodes for High-Performance Capacitive Deionization. *Environ Sci Technol* 50:13495-13501
- [84] Ma J, Zhang Y, Collins RN, Tsarev S, Aoyagi N, Kinsela AS, Jones AM, Waite TD (2019) Flow-Electrode CDI Removes the Uncharged Ca-UO₂-CO₃ Ternary Complex from Brackish Potable Groundwater: Complex Dissociation, Transport, and Sorption. *Environ Sci Technol* 53:2739-2747
- [85] Fang K, Gong H, He W, Peng F, He C, Wang K (2018) Recovering ammonia from municipal wastewater by flow-electrode capacitive deionization. *Chemical Engineering Journal* 348:301-309
- [86] Moreno D, Hatzell MC (2018) Influence of Feed-Electrode Concentration Differences in Flow-Electrode Systems for Capacitive Deionization. *Ind Eng Chem Res* 57:8802-8809
- [87] Park JE, Lee GB, Hwang SY (2021) Electrochemical Capacitance of Activated Carbons Regenerated using Thermal and Chemical Activation. *Journal of Electrochemical Science and Technology* 12:339-345
- [88] Linnartz CJ, Rommerskirchen A, Wessling M, Gendel Y (2017) Flow-Electrode Capacitive Deionization for Double Displacement Reactions. *ACS Sustain Chem Eng* 5:3906-3912
- [89] Zhang C, Ma J, He D, Waite TD (2018) Capacitive Membrane Stripping for Ammonia Recovery (CapAmm) from Dilute Wastewaters. *Environ Sci Technol Lett* 5:43-49
- [90] Zhang C, Ma J, Waite TD (2019) Ammonia-Rich Solution Production from Wastewaters Using Chemical-Free Flow-Electrode Capacitive Deionization. *ACS Sustain Chem Eng* 7:6480-6485
- [91] He C, Ma J, Zhang C, Song J, Waite TD (2018) Short-Circuited Closed-Cycle Operation of Flow-Electrode CDI for Brackish Water Softening. *Environ Sci Technol* 52:9350-9360
- [92] Xu L, Yu C, Mao Y, Zong Y, Zhang B, Chu H, Wu D (2021) Can flow-electrode capacitive deionization become a new in-situ soil remediation technology for heavy metal removal? *J Hazard Mater* 402:123568
- [93] Zhang X, Yang F, Ma J, Liang P (2020) Effective removal and selective capture of copper from salty solution in flow electrode capacitive deionization. *Environ Sci (Camb)* 6:341-350
- [94] Bian Y, Chen X, Lu L, Liang P, Ren ZJ (2019) Concurrent Nitrogen and Phosphorus Recovery Using Flow-Electrode Capacitive Deionization. *ACS Sustain Chem Eng* 7:7844-7850
- [95] Choi S, Chang B, Kang JH, Diallo MS, Choi JW (2017) Energy-efficient hybrid FCDI-NF desalination process with tunable salt rejection and high water recovery. *J Memb Sci* 541:580-586
- [96] Wang J, Liu C, Ding S, Yang Y (2025) Capacitive deionization in water treatment: A review of reactor dynamics, electrode materials, functional membranes, and modeling techniques. *Desalination* 600:118459
- [97] Ma J, Ma J, Zhang C, Song J, Dong W, Waite TD (2020) Flow-electrode capacitive deionization (FCDI) scale-up using a membrane stack configuration. *Water Res* 168:115186

- [98] Saif HM, Gebregeorgis TH, Crespo JG, Pawlowski S (2024) The influence of flow electrode channel design on flow capacitive deionization performance: Experimental and CFD modelling insights. *Desalination* 578:117452
- [99] Li Y, Ma J, Yang C, Niu J, Bian Y, Chen R, Zhang P, Zhang J, Liu C (2024) A novel flow electrode capacitive deionization device with spindle-shaped desalting chamber. *Front Environ Sci Eng* 18:40
- [100] Liu X, Shanbhag S, Bartholomew T V., Whitacre JF, Mauter MS (2021) Cost Comparison of Capacitive Deionization and Reverse Osmosis for Brackish Water Desalination. *ACS ES and T Engineering* 1:261-273
- [101] Alsaikhan K, Alsultan A, Alkhaldi A, et al (2023) Carbon Material-Based Flow-Electrode Capacitive Deionization for Continuous Water Desalination. *Processes* 11:195
- [102] Tauk M, Bechelany M, Lagerge S, Sstat P, Habchi R, Cretin M, Zaviska F (2023) Influence of particle size distribution on carbon-based flowable electrode viscosity and desalination efficiency in flow electrode capacitive deionization. *Sep Purif Technol* 306:122666
- [103] Rommerskirchen A, Linnartz CJ, Müller D, Willenberg LK, Wessling M (2018) Energy Recovery and Process Design in Continuous Flow-Electrode Capacitive Deionization Processes. *ACS Sustain Chem Eng* 6:13007-13015
- [104] Tan C, He C, Tang W, Kovalsky P, Fletcher J, Waite TD (2018) Integration of photovoltaic energy supply with membrane capacitive deionization (MCDI) for salt removal from brackish waters. *Water Res* 147:276-286
- [105] Chung HJ, Kim J, Kim DI, Gwak G, Hong S (2020) Feasibility study of reverse osmosis-flow capacitive deionization (RO-FCDI) for energy-efficient desalination using seawater as the flow-electrode aqueous electrolyte. *Desalination* 479:114326